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## 9<sup>th</sup> HIPS-NET Workshop Underground Hydrogen Storage

## Nazika Moeininia, Cindy Kleinickel, Hagen Bültemeier DBI Gas- und Umwelttechnik GmbH

### 9<sup>th</sup> HIPS-NET Workshop, Web Conference



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# Hydogen – Energy Carrier of the Future



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## Underground Gas Storage Europe – Overview



→ TOTAL working gas volume of natural gas in EUROPE 1572 TWh



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## Gas Storage Europe – Overview

#### Capacities by Type (Total Europe)

Type/Status	Operational				
	TWh	No.			
Aquifer	88,7	27			
Depleted field	761,7	87			
Rock Cavern	0,1	2			
Salt cavern	203,4	61			
VGS - multiple types	518,4				
Europe total	1572,2	177			

Data © GIE Storage Database 2021/07/14

#### Hydrogen Storage Potential (Theoretical)

- Factor 1.6 lower in terms of volume then natural gas
- Factor 3.5 lower in terms of energy then natural gas



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## Why (Underground-) Hydrogen Storage?



Speicherkapazität

Michael Sterner et al (2017): Energiespeicher, Springer Vieweg

#### Short-term storage

- Capacitors, coils (electric)
- Flywheel mass storage
- Batteries (electrochemical)
- Latent heat accumulators
- Compressed air storage
- Pumped storage plants (most of them)

#### Long-term storage

- Cavern storage
- Pore storage
- some thermal storages
- some pumped storage plants

→ Chemical energy storage systems are in the required order of magnitude with required ranges



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# Hydrogen Underground Storage – Status quo



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## Hydrogen underground storage - status quo

- Aspects affecting the underground storage of hydrogen (UGS)
  - Gas properties
    - » Hydrogen is smallest gas molecule
    - » Highly diffusible
    - Lower density, compressibility and energy content by volume compared to natural gas
  - Working gas volume (WGV) and stored energy
    - » Depending on gas density, compressibility and operating pressure range of UGS
  - Operation
    - » Pressures in the wellbore
    - » Flow velocities
  - Material and functionality of equipment
  - Quality demands: affected by
    - » hydrogen production process

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- » storage type (The storage of gases in geological formations leads to quality changes depending on the type of UGS and previous use)
- » as well as the transport of the hydrogen (pipeline)



#### © ESK GmbH, Z-Factor of Hydrogen (-blends)



© ESK GmbH, Maximum water content of Hydrogen (-blends)

## Hydrogen underground storage – status quo WGV and stored energy, example numbers for Germany

#### Basis

## $-p \cdot V = m \cdot R_i \cdot T \cdot Z(p,T)$

$$-V_N = V_{(p,T)} \cdot \frac{p_{res}}{p_N} \cdot \frac{T_N}{T_{res}} \cdot \frac{1}{Z(p,T)}$$

$$-WGV_{H_2} \cdot \frac{p_N}{p_{Res}} \cdot \frac{T_{Res}}{T_N} \cdot Z(p,T)_{H_2} = WGV_{NG} \cdot \frac{p_N}{p_{Res}} \cdot \frac{T_{Res}}{T_N} \cdot Z(p,T)_{NG}$$

#### Conversion

$$WGV_{H_2} = WGV_{Natural \ Gas} \cdot \frac{Z(p,T)_{Natural \ Gas}}{Z(p,T)_{H_2}}$$

	Cumulative storage capacity of existing UGS in Germany								
Types of UGS	Natural gas WGV	Natural gas WGV	H <sub>2</sub> -WGV	H <sub>2</sub> -WGV					
	Mio. m <sup>3</sup> i.N.	TWh	Mio. m <sup>3</sup> i.N.	TWh					
Pore UGS	8.615	92.671	5.952	18					
Cavern UGS	15.087	162.106	10.244	31					
Total	23.702	254.777	16.196	49					

**p**: pressure, **V**: Volume, **R**<sub>i</sub>: special gas constant, **T**: Temperature, **Z**: Z – Factor, **WGV**: Working gas volume

→ The amount of energy stored depends on the calorific value (approx. 3.5 x lower than natural gas)



## Operation: Pressure development in boreholes and impact on compressors

#### Static

 $- BHP = WHP \times e^{S}$ 

Example							
h	1200	m					
dv	0,069561077						
Temperature at WH	10	°C					
Temperature at BH	50	°C					
WHP	175	bar					
$Z_m = f(P_m, T_m)$	1,0716						
S	0,10185371						
BHP	193,76	bar					

**BHP**: Bottom Hole Pressure **WHP**: Well Head pressure **Hydrostatic Component**:  $s = \frac{g \cdot h}{T_m \cdot R_i \cdot Z_m}$ 



## Operation: Pressure development in boreholes and impact on compressors

 $BHP^2 = WHP^2 \times e^{2S} \pm \theta \dot{V}_n^2 \dot{V}_n$ 

Static component and dynamic friction losses:  $\theta = 1.137 \cdot 10^4 \cdot \frac{\lambda \cdot T_m^2 \cdot Z_m^2 (e^{2s} - 1)}{d^5}$ 



© DBI, Pressure development (Generic example)



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• 
$$\frac{T_2}{T_1} = \left(\frac{P_2}{P_1}\right)^{\frac{\kappa-1}{\kappa}}$$

- $P = \dot{m} \cdot c_p \cdot (T_2 T_1)$
- $\dot{Q} = \dot{m} \cdot c_p \cdot (T_3 T_2)$
- $T_1$  und  $P_1$ : Compressor inlet temperature & Pressure
- $T_2$  und  $P_2$ : Compressor outlet temperature & Pressure
- $T_3$ : Outlet temperature of cooler
- *Q*: Cooling Power, *m*: Mass flow rate & P: Power



<sup>©</sup> DBI, Compressor performance (Generic example )

- → Up to approx. 5 % by volume H<sub>2</sub>: isentropic exponent changes only insignificantly ( $\dot{m}\downarrow$ )
- → Up to approx. 20 vol.% H<sub>2</sub>:  $\dot{m}$  decreases and isentropic exponent changes significantly
- → Up to 100 % H<sub>2</sub>: Power decreases due to strongly decreased  $\dot{m}$



## Operation: cycles and convergence (cavern-UGS)

#### **Operation Cycles**

- Multi-cyclic possible in H<sub>2</sub>-operation
  - » Changed average cavern pressure
- Surface subsidence
  - » Change of P<sub>max</sub>, P<sub>min</sub>, P<sub>avg</sub>, Temperature, cycles during withdrawal process
  - » Change of mechanical properties of salt convergence
  - » WGV-Development





Scheme Subsidence as result of cavern convergence  $\circledcirc$  Sroka et. al, Freiberg, 2017

**Average**: 
$$P_{Avg} = \sum P_i t_i \text{ and } t_i = \frac{t}{365}$$



© DBI, Generic example

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## Material and functionality of equipment Main components of a UGS

Hydrogen has special thermodynamic, fluid dynamic, energetic, and corrosive properties that affect storage, operation, and equipment

- Surface facility
  - » Compressor
  - » Gas treatment

### - Well equipment

- » Tubing
- » Packer
- » SSV

### - Storage formation

 Microbial and geochemical processes, relevant for pore storage



Stylized P&ID surface facility © DBI-Gruppe





## Material and Functionality of Equipment



- → Cavern Storage: Evaluate material and function
- $\rightarrow$  Pore Storage: additional evaluation processes in the geological porous formation

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## Further Research demand



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#### Material assessment according to EIGA-guideline, no specific knowledge for APIsteels. Some practical short – mid-term experience was gathered in projects.

- » Austenitic metal grids
- » Carbon equivalent less than 0.35 %
- » Yield strength below 830 MPa
- » Phosphorus content  $\leq$  0.015 % and sulfur content  $\leq$  0.025%, etc.

We	ll completion	Material	C- content [%]	Mn- content [%]	Mo- content [%]	Cr- content [%]	V- content [%]	Ni- content [%]	Cu- content [%]	<b>C.E</b> [%]	Max. Sulfur content [%]	Max. Phosphorus content [%]	Yield strength [Mpa]	HRC [-]	<b>нв</b> [-]	Suitability
	Section 1, 32"									0						
	Section 2, 18 5/8"	N80								0	0,03	0,03	758			Does not come
	Section 3, 18 5/8"	K55								0	0,03	0,03	552			into contact with
Casing	Section, 13 3/8"	N80								0	0,03	0,03	758			the storage
	Section 5, 13 3/8"	N80								0	0,03	0,03	758			medium
	Section 6, 13 3/8"	N80									0,03	0,03	758			
	Section 7, 13 3/8"	N80								0	0,03	0,03	758			
Tubing	Steel pipe	C75	0,75	0,7	0,01	0,4	0	0,4	0	0,96166667	0,025	0,025	880		241	Not suitable
	Thread	C75	0,75	0,7	0,01	0,4	0	0,4	0	0,96166667	0,025	0,025	880		241	Not suitable
	Tubing Hanger	F6NM	0,05	1,5	0,5	13	0	4	0	2,81666667	0,015	0,04	520		245 - 309	suitable
	transition	AISI 4140	0,405	0,875	0,2	0,95	0	0	0	0,7425	0,04	0,04	655	22		Not suitable
Flow coupling	9 5/8"	AISI 4130	0,305	0,5	0,2	0,95	0	0	0	0,58	0,04	0,04	655	23		Not suitable
	7"	AISI 4140	0,405	0,875	0,2	0,95	0	0	0	0,7425	0,04	0,04	655	22		suitable



# For subsurface well completion materials, suitability of many components unclear yet. Some practical experiences exist.



→ DVGW-UGS-Kompendium (G 202143): 1st May 2022 – 31st August 2023
→ Casing below Packer – Current discussion



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# Further Research demand: suitability of porous UGS, processes in the reservoir

### Heterogenity of the reservoirs

- Hysteresis
- Gas mixing processes WGV CGV
- Dispersion
- Microorganisms
  - Present based on reservoir condition
- Salinity
  - Salinity $\uparrow \rightarrow H_2$  solubility  $\downarrow$

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- Hydrogen solubility in water
- Gas loss
  - » Biomethanation possible, if  $CO_2$  source present



© S. Bauer, "Underground Sun.Storage - Publizierbarer Endbericht - 3.1," RAG, Wien, 2017

→ Pore UGS are also important to achieve climate protection goals and to provide the required H2-storage capacities (until 2045)



# Further Research demand: suitability of porous UGS, processes in the reservoir

- Investigation of effects of gas properties (H<sub>2</sub> und H<sub>2</sub>-NG-blends)
  - Large difference in density
  - Large difference in viscosity
  - Large difference in compressibility
  - (competitive) gas solubility in (saline) water
- Main questions
  - Gas mixing behaviour, WGV (H<sub>2</sub>) CGV (Natural Gas)
    - » Structure of UGS, tilting angles, thickness, Aquifers,...
    - » Pore structure
    - » Well Locations and storage operation regime
  - Transmissivity
  - Diffusion, Dispersion
- $\rightarrow$  Clarification of Gas composition after withdrawal
- $\rightarrow$  required effort for treatment and purification



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# Further Research demand: suitability of porous UGS, processes in the reservoir

#### **Special topics**

- Microbial gas conversion processes
- Microbial growth, Pore-Plugging (bio-film generation)
- Geo-chemical rock alteration







 $CO_{2} + 4H_{2} \rightarrow CH_{4} + 2H_{2}O$   $2CO_{2} + 4H_{2} \rightarrow CH_{3}COOH + 2H_{2}O$   $SO_{4}^{2-} + 5H_{2} \rightarrow H_{2}S + 4H_{2}O$   $3Fe_{2}^{III}O_{3} + H_{2} \rightarrow 2Fe_{3}^{II}O_{4} + H_{2}O$ 



#### Time

Overview microbial processes in reservoirs © Parker et. al, 2018



# Thank you very much for your attention!

Your contact

## Nazika Moeininia

Project Manager/Reservoir Engineer

Tel.: +49 (0) 3731 4195 362 E-Mail: nazika.moeininia@dbi-gruppe.de

DBI Gas- und Umwelttechnik GmbH Karl-Heine-Straße 109/111 · D-04229 Leipzig

• www.dbi-gruppe.de



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→ DBI eigenes Berechnungstool zur Spannungs- und Stabilitätsberechnung



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#### Well load - Tubing subsystem vs. Casing subsystem - Cement - Formation



#### $\rightarrow$ Isotropic load in the tubing subsystem



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## Well Integrity

Stress calculation in borehole completions Casing - cement - formation subsystem





© DBI, Well load in subsystem Casing-cement-formation - Anisotropic

# → Contact pressure is difficult to calculate mathematically → numerical simulation is necessary



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## Bohrungsintegrität (Beispiel)



Teufe [m]	Anfahren <i>S<sub>t</sub></i> [-]	Einspeichern <i>S<sub>t</sub></i> [-]	Ausspeichern <i>S<sub>t</sub></i> [-]
0	1,92	1,92	2,56
1230	2,95	2,72	4,07

Beispiel: Ergebnisse Integritätsberechnung Tubing

$$S = \frac{\sigma_R}{\sigma_{V,Mi}} \le 1,25$$

© DBI, Radialspannungsverlauf des Systems Tubing-Casing-Zement-Gebirge (Beispiel)

#### $\rightarrow$ Prüfung bestehender Casing-Komplettierung auf Standsicherheit für H<sub>2</sub>-Betrieb



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